## Snow Survey Data for the Kuparuk Foothills

Hydrology Study: Spring 2007


Spring snowpack during dusk, UAF Staff
by
Sveta Berezovskaya, Jeff Derry, Douglas Kane, Robert
Geick, Michael Lilly, Dan White

July 2007

Kuparuk Foothills Hydrology Project
Report No. INE/WERC 07.17


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Sveta Berezovskaya ${ }^{1}$, Jeff Derry ${ }^{2}$, Douglas Kane ${ }^{1}$, Robert Geick ${ }^{1}$, Michael Lilly ${ }^{2}$, Dan White ${ }^{1}$

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## DISCLAIMER

The contents of this report reflect the views of the authors, who are responsible for the accuracy of the data presented herein. This research was funded by the Alaska Department of Transportation and Public Facilities (AKDOT\&PF). The contents of the report do not necessarily reflect the views of policies of the AKDOT\&PF or any local sponsor. This work does not constitute a standard, specification, or regulation.

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UNITS, CONVERSION FACTORS, WATER QUALITY UNITS, VERTICAL AND HORIZONTAL DATUM, ABBREVIATIONS AND SYMBOLS

Conversion Factors

| Multiply | By | To obtain |
| :---: | :---: | :---: |
|  | Length |  |
| inch (in.) | 25.4 | millimeter (mm) |
| inch (in.) | 2.54 | centimeter (cm) |
| foot (ft) | 0.3048 | meter (mm) |
| mile (mi) | 1.609 | kilometer (km) |
|  | Area |  |
| Acre | 43559.826 | square feet ( $\mathrm{ft}^{2}$ ) |
| Acre | 0.407 | hectare (ha) |
| square foot ( $\mathrm{ft}^{2}$ ) | 2.590 | square mile ( $\mathrm{mi}^{2}$ ) |
| square mile ( $\mathrm{mi}^{2}$ ) | 2.590 | square kilometer ( $\mathrm{km}^{2}$ ) |
|  | Volume |  |
| gallon (gal) | 3.785 | liter (L) |
| gallon (gal) | 3785 | milliliter (mL) |
| cubic foot ( $\mathrm{ft}^{3}$ ) | 23.317 | liter (L) |
| Acre-ft | 1233 | cubic meter ( $\mathrm{m}^{3}$ ) |
|  | Velocity and Discharge |  |
| foot per day (ft/d) | 0.3048 | meter per day ( $\mathrm{m} / \mathrm{d}$ ) |
| Square foot per day ( $\mathrm{ft}^{2} / \mathrm{d}$ ) | . 0929 | square meter per day ( $\mathrm{m}^{2} / \mathrm{d}$ ) |
| cubic foot per second ( $\mathrm{ft}^{3} / \mathrm{s}$ ) | 0.02832 | cubic meter per second ( $\mathrm{m}^{3} / \mathrm{sec}$ ) |
|  | Hydraulic Conductivity |  |
| foot per day (ft/d) | 0.3048 | meter per day ( $\mathrm{m} / \mathrm{d}$ ) |
| foot per day (ft/d) | 0.00035 | centimeter per second (cm/sec) |
| meter per day (m/d) | 0.00115 | centimeter per second (cm/sec) |
|  | Hydraulic Gradient |  |
| foot per foot (ft/ft) | 5280 | foot per mile (ft/mi) |
| foot per mile (ft/mi) | 0.1894 | meter per kilometer (m/km) |
|  | Pressure |  |
| pound per square inch ( $\mathrm{lb} / \mathrm{in}^{2}$ ) | 6.895 | kilopascal (kPa) |

## UNITS

For the purposes of this report, both English and Metric (SI) units were employed. The choice of "primary" units employed depended on common reporting standards for a particular property or parameter measured. Whenever possible, the approximate value in the "secondary" units was also provided in parentheses. Thus, for instance, snow density was reported in kilograms per cubic meter ( $\mathrm{kg} \mathrm{m}^{-3}$ ) followed by the approximate value in slugs per cubic feet (slug $\mathrm{ft}^{-3}$ ) in parentheses.

## Vertical Datum:

In this report, "sea level" refers to the National Geodetic Vertical Datum of 1929 (NGVD of 1929), a geodetic datum derived from a general adjustment of the first-order level nets of both the United States and Canada, formerly called Sea Level Datum of 1929.

Horizontal Datum:
The horizontal datum for all locations in this report is the North American Datum of 1983.

## Abbreviations, Acronyms, And Symbols

| AAS | Alaska's Arctic Slope |
| :--- | :--- |
| ADOT\&PF | Alaska Department of Transportation and Public Facilities |
| F | Fahrenheit $\left({ }^{\circ} \mathrm{F}\right)$. |
| ft | feet |
| GWS | Geo-Watersheds Scientific |
| kg | kilograms |
| $\mathrm{km}^{2}$ | square kilometers |
| m | meters |
| NGVD | National Geodetic Vertical Datum |
| NRCS | Natural Resources Conservation Service |
| NWIS | National Water Information System |
| QA | quality assurance |
| QC | quality control |
| Slug | slug |
| UAF | University of Alaska Fairbanks |
| USGS | U.S. Geological Survey |
| WERC | Water and Environmental Research Center |
| WWW | World Wide Web |
| YSI | Yellow Springs Instruments |

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# Snow Survey Data for the Kuparuk Foothills Hydrology Study: Spring 2007 

## 1. INTRODUCTION

This report discusses snow conditions that were observed during 2007 end-of-winter snow survey in the study area of the Kuparuk River basin. Field studies primarily focused on maximum snow water equivalent (SWE) accumulation during the 2006-2007 winter and the following snow melt. Field activities start at the end of April, because the snowpack virtually binds all precipitation falling during the period from October to April with no winter melt occurring on the Alaska’s Arctic Slope (AAS) (Benson et al., 1986). Deficiencies in determining snow precipitation and sublimation imply that measurements of snow accumulated on the ground provide the most reliable observational component of winter water budget.

Assessment of maximum snow accumulation is critical input to snow hydrology studies. Seasonal snowpack constitutes winter detention storage for precipitation, induces considerable differences in surface energy balance and results in soil desiccation of the organic layer overlying permafrost (Kane et al., 1978). Water contained in snowpack ensures that snowmelt is a major hydrological event each year. Peak discharge, resulting from snowmelt, is the highest for many rivers on the North Slope, particularly for the basins of the Sagavanirktok, Canning and Kuparuk Rivers. These rivers drain a large area that extends from the Brooks Range through the Northern Foothills and across the coastal plain before discharging into the Arctic Ocean. Snow starts contributing to runoff in the southern mountainous province in May and usually within a month melt is complete. Due to extremely high snowpack heterogeneity, knowledge on SWE spatial distribution is critical for understanding a river basin's hydrologic response during ablation.

This report presents snow water equivalent observational data for the eastern part of the Alaskan Arctic. It summarizes 2007 data collection procedure, accuracy of observations and their spatial distribution.


Figure 1. Geographical map of study area. Solid lines show major rivers; dashed lines represent approximate boundaries of the Coastal Plain, Foothills and Mountains regions.

## 2. AREA OF OBSERVATIONS

The study domain covers an 80 by 230 km region of the AAS that is bounded by the Brooks Range on the south and the Arctic Ocean on the north and includes the Kuparuk River basin (8 $140 \mathrm{~km}^{2}$ ). The southern and northern boundaries of the domain are at $68^{\circ} 28^{\prime}$ and $70^{\circ} 30^{\prime} \mathrm{N}$ latitude, respectively. The western and eastern boundaries of the domain are approximately at $150^{\circ} 30^{\prime}$ and $148^{\circ} 30^{\prime}$ W longitude, respectively. The total elevation range within the Kuparuk River basin is sea level to 1464 m ( 0 to 4800 ft ). The topography is characterized by flat northern portion, generally referred to as "Coastal Plain", followed by gently rolling hills and valleys extending to the south ("Foothills") and mountain ridges of the Brooks Range ("Mountains") (Figure 1).

Vegetation falls within a large region of sedge tussocks and mosses that cover much of northern Alaska. Occasional groupings of willows, approximately 40 cm high, occur in hillside water tracts and in the valley bottom. Riparian areas in the foothills are covered with shrubs (up to 2 m tall) and even trees in some areas (maximum 8 to 10 m ). The surface organic soils vary from live organic material at the surface to partially decomposed organic matter between 10 and 20 cm in depth. Silt, overlying a glacial till, makes up the mineral soil in the glaciated area (Kane et al, 1989). Overall, the topography and vegetation of the domain are representative of the AAS region.

## 3. SAMPLING METHODS

Our snow surveys are made at designated stations throughout the domain to determine the depth, vertically integrated density and water equivalent (Figure 2). Most of the sites, except for ablation measurements (see section 3.2), are visited once a year near the peak of snow accumulation, the last week of April. Our observations in the Foothills showed that snow never melts before last week of April. Also, March, April and May are typically the months of lowest precipitation and, therefore, there is not much accumulation between the surveys and ablation.


Figure 2. Location map of 2007 snow survey sites and meteorological stations.

In addition, meteorological stations are equipped with snow sensors that operate during the cold season and collect snow depth data at a point. Data can be collected in near real time or in the field directly from data logger.

### 3.1 Snow Survey

Our snow survey includes gravimetric SWE sampling and snow depth measurements collected over a 25 m by 25 m area; this technique is often referred to as "double sampling". The Alaskan snowpack is extremely heterogeneous (Benson and Sturm, 1993). Usually, double sampling yields an areal SWE estimate with a lower variance than is possible by collecting snow cores only, because considerably more snow depths than SWE measurements can be made in a time increment. Rovansek et al. (1993) showed that double sampling provides improved SWE estimates and recommended sampling 12 to 15 snow depths for each snow core. However, this optimal ratio of snow depths to water equivalent appeared to vary greatly (from 1 to 23), depending on weather and snow conditions. Currently, we use an optimal ratio of 10; that is, 50 depths accompany five snow cores.

Snow cores are sampled using fiberglass tube ("Adirondak") with an inside area of $35.7 \mathrm{~cm}^{2}$, equipped with metal teeth on the lower end to cut through dense layers of snow. The advantage of the Adirondak for shallow snowpack is that it has a larger diameter than many other types of snow tubes and thus provides a larger sample. To obtain a complete snow core, the Adirondak tube is pushed vertically through the snow while turning until soil is encountered; at this point the snow depth is recorded. The tube is then driven further into the organic layer and tipped sideways, retaining a vegetation plug that ensures the complete snow column was sampled. The vegetation plug is then removed and the snow is collected to be weighed later, in the laboratory. This procedure allows estimating both average snow density and snow water equivalent.

We use constant 50 m length for the snow depth course with a 1 m sampling interval along an Lshaped transect. Twenty five depth measurements are made on each leg of the L; this strategy is used to account for the presence of snowdrifts in the area of measurement. The directions of measurement are chosen randomly. Snow depth measurements are collected using a T-shaped
graduated rod (T-probe). The probe is simply pushed through the snow to the snow-ground interface.

Snow water equivalent is defined as
$S W E=\left(S D^{*} \rho_{s}\right) / \rho_{w}$
where $\rho_{s}$ is snow density, averaged from the 5 snow core samples, $\rho_{w}$ is water density and $S D$ is an average of 50 snow depths.

### 3.2 Snow Ablation

In addition to 2007 ablation data description, this report summarizes snowmelt observations conducted continuously since 1985 on a north-south transect along the Dalton Hwy.

### 3.2.1 Observation from 1985 to 2006

Measurement methods have changed over time as techniques have been modified to improve sampling accuracy. From 1985 to 1992 water equivalents were estimated from 10 randomly collected snow cores. These cores were sampled using Adirondak tubes and weighed using their mechanical scales, calibrated in inches of water. To overcome difficulties weighing samples in frequent high wind conditions, cores were often placed in zip-lock bags in the field and weighed indoors out of the wind using the Adirondak mechanical scale and after 1999 digital scales. Following Rovansek et al. (1993), double sampling technique was adopted in 1996 and continues to be used through the present (section 3.1). During the transition period (1993-1995), 5 to 20 snow cores were taken along with fifty snow depths. Snow depths have been measured using a variety of devices such as: Adirondak snow tube, avalanche probes, T-handled graduated probes, MagnaProbe, ski poles and rods with added graduated scales.

Number of observational sites has also changed over the time (Table 1). In 1985, the only sites where snow water equivalent and ablation were observed, were in the Imnavait Creek Basin. Sagwon Hill (SH) and Franklin Bluffs (FR) sites were added in 1986. Snow surveys at the

Sagwon site were made near the meteorological site, usually just east of the 3 or 10 meter tower away from the NRCS Wyoming snow gauge leeward drift. The Franklin Bluffs site was located from 1986 through 1998 adjacent to the meteorological site 1 km east of the Dalton Highway. In 1999 the snow survey and ablation site was moved west approximately 300 meters from the highway. Betty Pingo Site on the Pruhoe Bay Oilfield was established in 1992. This snow survey site is located near the NRCS Wyoming snow gauge about 200 meters north of the Kuparuk Pipeline Road between P-Pad and Gathering Center 2. Upper Kuparuk, Happy Valley and West Dock snow survey and ablation sites were added in 1999.

Table 1. Summary of snow ablation sites.

| Site Name | Period of Record | Comments |
| :---: | :---: | :---: |
| Betty Pingo | 1993 to 2007 | Surveyed near NRCS Wyoming gauge |
| Franklin Bluffs | 1987 to 2007 | Surveyed near Met site 1983 to 1998, snow site moved |
|  |  | west 700 meters along access road 1999 to 2007. |
| Happy Valley | 1999 to 2007 | Survey site 150 meters west of Dalton Highway near |
|  |  | Happy Valley Airfield. |
| Imnavait Basin | 1985 to 2007 | Snow ablation measured at 4 sites on west-facing slope at |
|  |  | mid basin 1985 to 1988, and at a 6 site mid-basin transect |
|  |  | 1989 to 1997 and at a 6 sites transect along UTM |
|  |  | 612800 northing. |
| Sagwon Hill | 1987 to 2007 | Adjacent to the Sagwon Meteorological Site |
| West Dock | 1999 to 2007 | 150 meters east of West Dock - GC1 Road approximately |
|  |  | one mile south of West Dock Meteorological Site. |
| Upper Kuparuk | 1999 to 2007 | Adjacent to the Upper Kuparuk Meteorological Site |

Imnavait Creek basin (IB) differs from others in that it has the longest period of records and detailed observations. There were always several sites sampled across the basin to capture basin average snow water equivalent. From 1985 through 1997 Imnavait Basin snow water equivalent was determined from a transect made across the basin perpendicular to the stream channel. At this time snow ablation was tracked only at west-facing slope adjacent to 4 runoff plots (Hinzman, 1990). In 1989, 2 additional sites were added in the valley bottom and on the eastfacing slope of the basin. To provide consistent identification of sites, the transect runs at 7612800 northing (NAD27, UTM6) since 1999.

### 3.2.2 Ablation observations in 2007

Snow ablation at all sites, described above (section 3.2.1), is observed to date. During 2007 snow melt, SWE observations were conducted at the Upper Kuparuk station (UKmet), Sagwon Hill (SH), Franklin Bluffs (FR), Betty Pingo (Betty), Happy Valley (HV), West Dock (WD) and at six sites across the Imnavait basin (IB1-IB6). Snow courses using double sampling technique (see section 3.1) have been made daily or every other day to capture the net volumetric decrease in SWE. The only difference from the end of winter snow survey is that the snow depth course has an assigned location, because of numerous repeated measurements.

### 3.3 Snow-Depth Sensors

Ten meteorological stations located on the North Slope/ Kuparuk Foothills Project are equipped with a Sonic Ranger 50 (SR50) snow depth sensors. Four of these stations are established by the Kuparuk River/ Foothills project (DFM1, DFM2, DFM3, DFM4) (Figure 2). Other stations are maintained by WERC as part of the NSF project. The SR50 probe uses ultrasonic pulses to measure the distance from the sensor to the snow surface. Basically, the SR50 sends out an ultrasonic pulse and times how long it takes to sense the pulse echo. Although the SR50 can measure the distance to any reflective surface like the ground or water, the sensitivity of the SR50 is designed for use in measuring distance to a snow surface.

The basic idea for measuring snow depth with the SR50 is simple subtraction. When there is no snow on the ground, the distance measured is the sensor's height above the ground. When snow has accumulated under the sensor the distance measured is to the snow surface. The difference between distance to the ground and distance to the snow surface yields snow depth. For example, if the sensor's height above the ground is 50 inches and 10 inches of snow accumulates, the new distance to surface will be 40 inches. Hence, 40 inches subtracted from 50 inches gives depth of the snow under the sensor of 10 inches.

The SR50 sampling method is point data that typically records measurements at hourly intervals. Thus, the SR50 has a low spatial coverage yet a high temporal resolution, while snow survey data has at higher spatial coverage yet at low temporal resolution. Snow sensor data used in conjunction with snow survey data can enhance and expand the limitations of each sampling method.

## 4. ACCURACY OF OBSERVATIONS

The problems of measuring and processing any observational data are critical to realize and address. This section provides an accuracy assessment of our observations, so the data can be utilized properly.

### 4.1 Snow-Water Equivalent

Core SWE often underestimates the water amount contained in the snowpack (our observations, personal communication with M. Sturm). In attempting to quantify underestimation in shallow tundra snowpack conditions, Woo et al. (1997) showed that a larger tube diameter increases the accuracy of density determination; he also showed that the Canadian sampler (similar to the Adirondak in diameter) captures snow density within 5\% of snow pit estimates. Our comparison of Adirondak to snow pit density give similar results.

The accuracy of a single snow depth measurement is difficult to quantify. In the area of welldeveloped organics on top of the mineral soils, snow depth is often overestimated (Berezovskaya
and Kane, 2007). While measuring, the probe can easily penetrate low-density organic material, so this additional depth is often inadvertently incorporated into the snow depth measurement. Any type of correction to existing snow depth records is difficult to perform, because the error varies strongly from observer to observer, as well as depending on the snow and soil conditions at each site.

Whereas snow depths show a systematic overestimation error, snow core densities tend to be close to, or to underestimate, SWE. The difficulty in SWE accuracy interpretations is that actual, accurate SWE is unknown. Comparing different sampling methods, Berezovskaya and Kane (2007) concluded that SWE of the tundra snow estimated with double sampling technique has error of $\pm 10 \%$.

### 4.2 Snow-Depth Sensors

Diligent field practices are essential for accurate measurements. After the sensor is installed and subsequently every time the station is visited, the distance from the bottom of the sensor to five points (four distances at $20^{\circ}$ angles around sensor, and one directly underneath) on the ground is measured. When snow is on the ground, five depth measurements and the distance from the sensor to the snow surface are obtained. This information is crucial for post processing data correction.

Adjustments to data may vary according to the error tolerance and goals of the investigation, for this report QA/QC procedures are outlined below:

- Establish a baseline value that represents no snow on the ground.
- Manually review data (graphically), and replace erroneous values with the average from the first and last data value that is deemed reasonable.
- Adjust data to fit observed values in the field.
- Lastly, smooth the data and omit smaller, sporadic, data values. If the difference between a data point and the prior data point is greater than 1.5 cm , and/or the difference between a data point and the following data point is greater than 1.5 cm , then replace the data point
with the average of the prior 5 hours and following 5 hours of data. A 10-hour average helped smooth out blowing snow events and cold periods that may have altered readings.
- As to avoid an abrupt transition during accumulation and/or ablation periods, incrementally adjust data over a period of days.

Potential inherent errors exist. For example, since the speed of sound in air is affected by the temperature of the air it is traveling in, an air temperature measurement is required to correct the distance reading. Inaccuracies can be caused by poor calibration and/or neglecting periodic maintenance requirements. Physically related errors include blowing snow creating spurious data readings, difficulty in establishing a zero point due to tussocks, low shrubs, grass, etc., ground heave altering sensor height, changes in sensor height and angle as well as cable breakages due to wildlife curiosities.

## 5. SPATIAL DISTRIBUTION OF SNOW SITES

Snow survey sites are chosen to represent snow characteristics over a wide range of vegetation and terrain conditions. Snow water equivalents are measured at elevations from sea level to 3674 $\mathrm{ft}(0$ to $\sim 1120 \mathrm{~m}$ ) in the Kuparuk River basin (Appendix A1-A3).

There are two distinctly different snow regimes across the Kuparuk basin, uplands and coastal (Liston and Sturm, 2002). To determine regional SWE, snow sites are classified as the Coastal Plain and uplands, the latter is separated into Foothills and Mountains. The coastal sites are the sites located below elevation isoline of $500 \mathrm{ft}(152 \mathrm{~m})$ and those above are referred to as uplands sites. Uplands snow sites are, in turn, separated into foothills and mountains based on elevation and surrounding topography (Appendix A1-A3). Elevation only is not representative for this purpose, because in the mountains most of the snow survey sites are located in the valley bottoms where helicopter can safely access the site.

Overall, 141 sites were visited in 2007. This number includes 100 sites within the frame of the Foothills project and 41 sites within the Bullen Point project. 7 of the Foothills project sites are located in the Mountains, 45 sites are in the Foothills and 48 sites are on the Coastal Plain.

## 6. SUMMARY OF SNOW OBSERVATIONS

Average of Coastal Pain snow densities ( 0.458 slug $\mathrm{ft}^{-3} / 236 \mathrm{~kg} \mathrm{~m}^{-3}$ ) are similar to the Foothills ( 0.460 slug $\mathrm{ft}^{-3} / 237 \mathrm{~kg} \mathrm{~m}^{-3}$ ) and less than the Mountains ( $0.504 \mathrm{slug} \mathrm{ft}^{-3} / 260 \mathrm{~kg} \mathrm{~m}^{-3}$ ) (Appendix B1-B3).

The average of Coastal Plain SWE is 3.2 in ( 8.2 cm ), and snow depth is 14.0 in ( 35.5 cm ). Foothills average snow water equivalent is 4.6 in ( 11.6 cm ), and snow depth average is 19.3 in ( 49.0 cm ). Mountains average snow water equivalent ( $2.5 \mathrm{in} / 6.3 \mathrm{~cm}$ ) and snow depths ( 9.7 in / 24.7 cm ) are generally lower than those at the Coastal Plain and Foothills. By the end of April Foothills have the highest SWE accumulation and Mountains have the lowest average SWE.

Observations at the Coastal Plain have then been corrected for the heavy snowfalls in early May (section 8). The adjusted average Coastal Plain SWE is 3.6 in ( 9.1 cm ). SWE data before and after storm are listed in Appendix B4.

Overall, snow accumulation over domain is less than average, 90 \% of 8 -years average (20002007) and higher than last year (108 \%) (Table 2). Mountains, Foothills and Coastal Plain regions have accumulated $70 \%, 102 \%$ and $96 \%$ of average SWE (Table 3). There is only one other source of long-term SWE records collected by NRCS along the Dalton highway. NRCS reports 73 \% of average snow accumulation for the Coastal Plain in 2007 (McClure R., 2007).

Table 2. The Kuparuk River snow water equivalent: 2000 - 2007.

|  | Mountains |  |  | Foothills |  |  | Coastal Plain |  |  | Kuparuk basin |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SWE |  | Number <br> of sites | SWE |  | Number <br> of sites | SWE |  | Number <br> of sites | SWE |  | Number <br> of sites |
| YEAR |  |  |  |  |  |  |  |  |  |  |  |  |
|  | cm | in |  | cm | IN |  | cm | in |  | cm | in |  |
| 2000 | 9.3 | 3.7 | 2 | 12.3 | 4.8 | 36 | 9.9 | 3.9 | 20 | 10.5 | 4.1 | 58 |
| 2001 | 8.3 | 3.3 | 3 | 11.8 | 4.6 | 36 | 8.4 | 3.3 | 36 | 9.5 | 3.7 | 75 |
| 2002 | 6.6 | 2.6 | 2 | 11 | 4.3 | 32 | 9.4 | 3.7 | 34 | 9 | 3.5 | 68 |
| 2003 | 14.7 | 5.8 | 3 | 12.2 | 4.8 | 36 | 11.2 | 4.4 | 32 | 12.7 | 5.0 | 71 |
| 2004 | 8.8 | 3.5 | 3 | 11.3 | 4.4 | 28 | 9.2 | 3.6 | 14 | 9.8 | 3.9 | 45 |
| 2005 | 11.6 | 4.6 | 1 | 11.4 | 4.5 | 33 | 8.9 | 3.5 | 26 | 10.6 | 4.2 | 60 |
| 2006 | 6.7 | 2.6 | 7 | 8.9 | 3.5 | 39 | 9.5 | 3.7 | 41 | 8.4 | 3.3 | 87 |
| 2007 | 6.3 | 2.5 | 7 | 11.5 | 4.5 | 43 | 8.2 | 3.2 | 50 | 9.1 | 3.6 | 100 |
| Average | 9.0 | 3.6 |  | 11.3 | 4.5 |  | 9.3 | 3.7 |  | 9.9 | 3.9 |  |

Table 3. 2007 snow water equivalent analysis.

| Region | Number of <br> sites | SWE |  | Percent of last <br> year | Percent of <br> average |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  |  | Cm | in |  |  |
| Mountains | 7 | 6.3 | 2.5 | 94 | 70 |
| Foothills | 45 | 11.5 | 4.5 | 129 | 102 |
| Coastal Plain |  | 8.1 | 3.2 | 85 | 87 |
|  |  | $\left(9.1^{*}\right)$ | $\left(3.6^{*}\right)$ | $\left(94^{*}\right)$ | $\left(96^{*}\right)$ |
| The Kuparuk River | 100 | 8.6 | 3.4 | 102 |  |
| basin |  | $\left(9.0^{*}\right)$ | $\left(3.6^{*}\right)$ | $\left(108^{*}\right)$ | $\left(90^{*}\right)$ |

* indicates an adjusted SWE (see section 8)


## 7. SUMMARY OF SONIC SNOW-DEPTH MEASUREMENTS

Three out of eight meteorological stations had continuous, good quality snow sensor data from the accumulation and ablation 2006-2007 season: Northwest Kuparuk (DFM4), the North White Hills (DFM3), and the South White Hills (DFM1) stations (Figure 3-5). DFM 2 station records have not been analyzed, because sensor indicated no snow. This station is located on the top of the ridge, where snow is eroded due to persisting strong winds. Sonic snow depth records at the other three stations were adjusted to account for field observations and anomalous data points (section 3.3). As an example, the Northwest Kuparuk Station demonstrates data before and after it was corrected for periods when no snow was on the ground as well as differences with observed snow depth (Figure 5). Correction procedure for South White Hills station did not help to reduce the noise in February to May records, so the data should be interpreted with caution. Possible reasons for this noise can be attributed to snow being blown into or under the sensor, obstructions on the ground, sensor malfunction and calibration issues.

South White Hills, DFM1, Meteorological Station


Figure 3. Corrected snow depth from Sonic Range S50 sensor installed at the South White Hills,
DFM1 meteorological station.


Figure 4. Corrected snow depth from Sonic Range S50 sensor installed at the North White Hills, DFM3 meteorological station.


Figure 5. Corrected snow depth from Sonic Range S50 sensor installed at Northwest Kuparuk, DFM4 meteorological station..

The maximum snow depth during the winter was about 20 cm at the North White Hills station and about 40 cm at the Northwest Kuparuk and South White Hills stations. Sonic sensor measurements are made at a point, so they are not always representative of surrounding snow cover depth. Fifty snow depth measurements taken at the nearest snow survey sites in May 2007 provide snow depth variability within 37 to 89 cm for the North White Hills, 32 to 76 cm for the Northwest Kuparuk, and 29 to 70 cm for the South White Hills. Sensor depth measurements are either close to the lower range or slightly less (North White Hills) than the minimum observed snow survey depth.

The advantage of snow sensor information is its high temporal resolution, which can capture the timing and relative magnitude of snow events. Our records show that snow accumulation began approximately at the end of September 2006 for the North White Hills site and early to midOctober 2006 for the Northwest Kuparuk and South White Hills sites. Several major snow
deposition and erosion events can be distinguished during the 2006-2007 season (Figure 3-6). Significant snow accumulation at the Northwest Kuparuk and South White Hills occurred last week of October, 2006 and, then, first week of December, 2006. During the week of January 815 2007, the Northwest Kuparuk's snow depth decreased by $50 \%$ and North White Hills decreased by $95 \%$. Decrease in snow depth is usually caused by strong winds that scour snow from open exposed areas (i.e. ridges and windward slopes) and deposit in the lee of the bluffs and other topographical or vegetation obstructions. All stations show snow accumulation during late March - early April and, then a response of various magnitudes to the late spring storm occurring approximately from May 6 to May 10, 2007. For all three stations, snow was no longer on the ground by June 8 to 12, 2007.

## 8. SUMMARY OF SPRING STORM

Following the initiation of April snow surveys, a storm event occurred approximately from May 5 to May 8, 2007. It brought heavy snowfalls and caused an additional snow accumulation throughout the Coastal Plain. The dominant wind direction was the northeast. Snow accumulation occurred from May 6 to May 8 in the Kuparuk River basin, roughly a day later than sites located in the Bullen Point Region to the east. Inclement weather before, during, and after the storm delayed accessing coastal survey sites via helicopter the majority of the first part of May.

To assess the storm impact on maximum SWE, we compared observations collected before and after this storm (Table 4). The difference was used 1) to localize the area of impact and 2) to adjust maximum winter snow accumulation (Appendix B4).

The evaluation considers the change in SWE at snow survey sites and meteorological stations. To convert snow sensor depth to SWE, an average density of $230 \mathrm{~kg} / \mathrm{m}^{3}$ from snow surveys taken near the same time and location is used. Data show a large spatial extent of the storm affecting survey sites; West Dock, Betty Pingo, Franklin Bluffs, as well as meteorological stations DFM 4 and DFM 3. An accumulation gradient from north to south is seen for the Coastal Plain (Table 4), with higher accumulation in the north decreasing towards the south.

Data also show a transitional zone in this north/south gradient occurring in the White Hills (WK10 site) and Sagwon Hills. Gradual SWE increase in the foothill and mountain areas (Upper Kuparuk and Imnavait Creek) is unlikely caused by the same storm extended into the upland areas. Through the direct snow observations, we would localize the area of spring storm impact to the Coastal Plain only.

Table 4. Observed SWE before and after spring storm. Sites listed in order by location going from north to south. Stations in bold indicate location is on the Coastal Plain.

| Site | Data | SWE before storm | SWE after storm | Difference |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | source | Date | cm | Date | cm | $\%$ |
| West Dock | Snow survey | $4 / 24$ | 5.8 | $5 / 13$ | 6.5 | 11 |
| Betty Pingo | Snow survey | $4 / 25$ | 6.5 | $5 / 13$ | 9.3 | 30 |
| DFM 4 | Snow sensor | $5 / 6$ | 5.9 | $5 / 9$ | 7.9 | 26 |
| Franklin Bluffs | Snow survey | $4 / 27$ | 6.6 | $5 / 17$ | 8.7 | 24 |
| DFM 3 | Snow sensor | $5 / 5$ | 2.5 | $5 / 8$ | 3.0 | 15 |
| WK 10 | Snow survey | $4 / 29$ | 12.4 | $5 / 9$ | 8.5 | -46 |
| Sagwon | Snow survey | $4 / 25$ | 7.5 | $5 / 17$ | 7.3 | -3 |
| DFM1 | Snow sensor | $5 / 5$ | 6.9 | $5 / 9$ | 7.5 | 9 |
| Happy Valley | Snow survey | $4 / 25$ | 7.3 | $5 / 17$ | 8.1 | 10 |
| Upper Kuparuk | Snow survey | $4 / 24$ | 11.9 | $5 / 16$ | 14.2 | 16 |
| Imnavait Creek | Snow transect | $4 / 25$ | 12.3 | $5 / 12$ | 11.3 | -9 |

The SWE increase on the Coastal Plain as a result of the storm ranges from $11 \%$ to $30 \%$. Snow surveys conducted prior to the storm event were grouped relative to their position to the West Dock, Betty Pingo, Franklin Bluffs, DFM4 and DFM3 sites (Figure 2). Correction factor,
derived as a ratio of SWE measured after storm to SWE measured before storm, was applied to each group (Appendix B4). Adjusted SWE result in an average SWE for the Coastal Plain to be 8.9 cm (3.5 in), or a 9 \% increase.

## 9. SUMMARY OF ABLATION OBSERVATIONS

The ablation window varies greatly depending on meteorological conditions and snowpack depth. The start of spring snowmelt usually occurs in the southern part first (Imnavait Basin, Upper Kuparuk sites) and a week or two later snow starts melting on a coastal plain (Franklin Bluffs, Betty Pingo and West Dock). Onset of ablation in 2007 varies from May 14 ${ }^{\text {th }}, 2007$ at the Imnavait Basin and Upper Kuparuk to May $27^{\text {th }}-$ May $30^{\text {th }}$, 2007 at northern sites with an average of 5 days to complete the melt (Figure 6). The Imnavait Basin ablation curve differs in that it is an average of six sites across the basin. Within a few days of sustained melt the entire watershed becomes a patchwork of snow covered and bare tundra. The west-facing slope melts off sooner than the rest of the watershed, because it retains less snow and has more direct solar radiation in the afternoon when air temperatures are highest (Hinzman et al., 1996). In contrast, the east-facing slope has deeper snowpack and receives its maximum irradiance in the morning while convective heat transfer is smaller. 10 days were required to complete ablation in the Imnavait watershed. Snowpack across the entire Kuparuk River basin melted off within three weeks from May $14^{\text {th }}$ to June $5^{\text {th }}, 2007$.


Figure 6. Snow ablation curves at the foothills (red and green lines) and on the coastal plain (blue lines). Imnavait basin shows SWE, averaged from six sites across the basin.

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APPENDIX A. LIST OF THE SNOW SURVEY SITES IN 2007

Appendix A1. Elevation and coordinates of the sites located in the Mountains

| № | ID | ELEV <br> m |  | LAT <br> decimal degree |
| :---: | :---: | :---: | :---: | :---: |

Appendix A2. Elevation and coordinates of the sites located in the Foothills

| № | ID | $\begin{gathered} \text { ELEV } \\ \mathrm{m} \end{gathered}$ | LAT <br> decimal degree | LON decimal degree |
| :---: | :---: | :---: | :---: | :---: |
| 1 | UK01 | 912 | 68.5849 | -149.306 |
| 2 | UK02 | 834 | 68.6010 | -149.338 |
| 3 | UK03 | 827 | 68.5639 | -149.335 |
| 4 | UK04 | 908 | 68.5335 | -149.231 |
| 5 | UK07 | 848 | 68.5489 | -149.311 |
| 6 | UK08 | 968 | 68.5222 | -149.338 |
| 7 | UK09 | 763 | 68.6241 | -149.379 |
| 8 | UK10 | 801 | 68.6173 | -149.384 |
| 9 | UK11 | 796 | 68.6215 | -149.360 |
| 10 | UK12 | 904 | 68.6007 | -149.425 |
| 11 | UK13 | 937 | 68.5899 | -149.416 |
| 12 | UK15 | 951 | 68.5540 | -149.373 |
| 13 | UK18 | 981 | 68.5187 | -149.328 |
| 14 | Ukmet | 778 | 68.6374 | -149.404 |
| 15 | SM01 | 732 | 68.7879 | -149.087 |
| 16 | SM02 | 680 | 68.7956 | -149.158 |
| 17 | SM03 | 651 | 68.8122 | -149.284 |
| 18 | SM04 | 612 | 68.8336 | -149.456 |
| 19 | SM05 | 568 | 68.8565 | -149.733 |
| 20 | SM06 | 609 | 68.7521 | -149.539 |
| 21 | Happy Valley | 314 | 69.1519 | -148.839 |
| 22 | HV1 | 365 | 69.1682 | -149.155 |
| 23 | HV2 | 353 | 69.1667 | -149.162 |
| 24 | HV3 | 386 | 69.1816 | -149.390 |
| 25 | HV4 | 308 | 69.2007 | -149.558 |
| 26 | HV5 | 179 | 69.2937 | -150.284 |
| 27 | HV6 | 218 | 69.2756 | -150.087 |
| 28 | Wkmet | 159 | 69.4259 | -150.342 |
| 29 | WK1 | 218 | 69.4265 | -148.872 |
| 30 | WK2 | 226 | 69.4278 | -149.038 |
| 31 | WK3 | 174 | 69.4291 | -149.298 |
| 32 | WK4 | 203 | 69.4269 | -149.461 |
| 33 | WK5 | 197 | 69.4269 | -149.457 |
| 34 | WK6 | 195 | 69.5199 | -149.262 |
| 35 | WK8 | 173 | 69.4576 | -149.953 |
| 36 | WK9 | 401 | 69.4826 | -149.797 |
| 37 | WK10 | 214 | 69.6173 | -149.384 |
| 38 | Sagwon | 275 | 69.4262 | -148.691 |
| 39 | H02 | 172 | 69.8020 | -150.384 |
| 40 | IB | 897 | 68.6134 | -149.318 |
| 41 | MI6 | 179 | 69.5344 | -148.599 |
| 42 | MI7 | 177 | 69.4887 | -148.568 |
| 43 | DFR1 | 508 | 69.0726 | -149.515 |
| 44 | DFM2 | 337 | 69.4865 | -149.821 |
| 45 | DFM1 | 293 | 69.2007 | -149.558 |

Appendix A3. Elevation and coordinates of the sites located on the Coastal Plain

| № | ID | $\begin{gathered} \text { ELEV } \\ \mathrm{m} \end{gathered}$ | LAT decimal degree | LON decimal degree |
| :---: | :---: | :---: | :---: | :---: |
| 1 | West Dock | 5 | 70.3602 | -148.570 |
| 2 | Franklin Bluffs | 71 | 69.8886 | -148.775 |
| 3 | FB1 | 71 | 69.8828 | -148.839 |
| 4 | FB2 | 64 | 69.9108 | -148.992 |
| 5 | FB3 | 58 | 69.9316 | -149.156 |
| 6 | FB4 | 52 | 69.9676 | -149.351 |
| 7 | FB5 | 42 | 70.0113 | -149.283 |
| 8 | FB6 | 38 | 70.0667 | -149.160 |
| 9 | FB7 | 32 | 70.1160 | -149.101 |
| 10 | FB8 | 34 | 70.0960 | -148.987 |
| 11 | FB9 | 34 | 70.0710 | -148.878 |
| 12 | FB10 | 40 | 70.0451 | -148.758 |
| 13 | P01 | 12 | 70.2955 | -148.937 |
| 14 | P02 | 15 | 70.2614 | -148.940 |
| 15 | P03 | 11 | 70.2744 | -148.891 |
| 16 | P04 | 12 | 70.2601 | -148.821 |
| 17 | P05/Betty | 15 | 70.2532 | -148.772 |
| 18 | P06 | 12 | 70.2562 | -148.670 |
| 19 | P07 | 12 | 70.2566 | -148.716 |
| 20 | P08 | 12 | 70.2486 | -148.604 |
| 21 | MI1 | 48 | 70.0032 | -148.679 |
| 22 | MI2 | 60 | 69.9336 | -148.768 |
| 23 | MI3 | 90 | 69.7950 | -148.736 |
| 24 | MI4 | 90 | 69.7130 | -148.716 |
| 25 | MI5 | 140 | 69.6050 | -148.649 |
| 26 | H01 | 113 | 69.5687 | -150.448 |
| 27 | H03 | 124 | 69.9467 | -149.920 |
| 28 | H04 | 77 | 69.9000 | -149.750 |
| 29 | H05 | 90 | 69.8000 | -149.750 |
| 30 | L30 | 73 | 69.7255 | -149.626 |
| 31 | L31 | 73 | 69.7730 | -149.492 |
| 32 | L34 | 116 | 69.6576 | -148.858 |
| 33 | NK4 | 101 | 69.7307 | -148.966 |
| 34 | WC1 | 127 | 69.6179 | -148.812 |
| 35 | WK7 | 137 | 69.4243 | -150.315 |
| 36 | DFM3 | 84 | 69.7149 | -149.470 |
| 37 | DFM4 | 124 | 69.9475 | -149.917 |
| 38 | KDA | 3 | 70.3326 | -149.941 |
| 39 | MSB | 3 | 70.1931 | -149.237 |
| 40 | LFH0701-L | 87 | 69.8468 | -149.727 |
| 41 | LFH0701 | 87 | 69.8468 | -149.727 |
| 42 | LFH0703-L | 83 | 69.7660 | -149.416 |
| 43 | LFH0703 | 83 | 69.7660 | -149.416 |
| 44 | LFH0702-L | 97 | 69.7038 | -149.813 |
| 45 | LFH0702 | 97 | 69.7038 | -149.813 |
| 46 | LFH0705-L | 95 | 69.7495 | -149.256 |
| 47 | LFH0705 | 95 | 69.7495 | -149.256 |
| 48 | LFH0704 | 83 | 69.7667 | -149.413 |

APPENDIX B. AVERAGE SNOW DENSITY, SNOW DEPTH AND SNOW WATER EQUIVALENT

Appendix B1. Summary for the sites located in the Mountains

| № | ID | SWE |  | SNOW DEPTH |  | SNOW DENSITY |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | cm | in | cm | in | ${\mathrm{kg} / \mathrm{m}^{3}}^{\text {slug } / \mathrm{ft}^{3}}$ |  |
| 1 | UK05 | 4.3 | 1.7 | 23.7 | 9.3 | 179 | 0.347 |
| 2 | UK06 | 4.9 | 1.9 | 16.4 | 6.5 | 301 | 0.584 |
| 3 | UK14 | 7.4 | 2.9 | 31.5 | 12.4 | 233 | 0.452 |
| 4 | UK16 | 3.2 | 1.3 | 10.7 | 4.2 | 299 | 0.580 |
| 5 | UK17 | 4.8 | 1.9 | 17.3 | 6.8 | 278 | 0.539 |
| 6 | UK19 | 8.9 | 3.5 | 32.4 | 12.8 | 276 | 0.535 |
| 7 | UK20 | 10.4 | 4.1 | 41.0 | 16.1 | 253 | 0.491 |
|  | Average | $\mathbf{6 . 3}$ | $\mathbf{2 . 5}$ | $\mathbf{2 4 . 7}$ | $\mathbf{9 . 7}$ | $\mathbf{2 6 0}$ | $\mathbf{0 . 5 0 4}$ |

Appendix B2. Summary for the sites located in the Foothills.

| № | ID | SWE |  | SNOW DEPTH |  | SNOW DENSITY |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | cm | in | cm | in | $\mathrm{kg} / \mathrm{m}^{3}$ | slug/ft ${ }^{3}$ |
| 1 | UK01 | 10.2 | 4.0 | 43.2 | 17.0 | 235 | 0.456 |
| 2 | UK02 | 10.1 | 4.0 | 44.8 | 17.6 | 227 | 0.440 |
| 3 | UK03 | 12.6 | 5.0 | 58.1 | 22.9 | 216 | 0.419 |
| 4 | UK04 | 6.0 | 2.4 | 22.0 | 8.7 | 272 | 0.528 |
| 5 | UK07 | 12.9 | 5.1 | 59.3 | 23.3 | 217 | 0.421 |
| 6 | UK08 | 3.0 | 1.2 | 11.1 | 4.4 | 268 | 0.520 |
| 7 | UK09 | 11.3 | 4.4 | 47.8 | 18.8 | 236 | 0.458 |
| 8 | UK10 | 16.3 | 6.4 | 72.2 | 28.4 | 255 | 0.495 |
| 9 | UK11 | 13.3 | 5.2 | 56.4 | 22.2 | 237 | 0.460 |
| 10 | UK12 | 7.7 | 3.0 | 32.5 | 12.8 | 237 | 0.460 |
| 11 | UK13 | 10.6 | 4.2 | 39.9 | 15.7 | 266 | 0.516 |
| 12 | UK15 | 10.6 | 4.2 | 40.1 | 15.8 | 265 | 0.514 |
| 13 | UK18 | 6.0 | 2.4 | 24.2 | 9.5 | 247 | 0.479 |
| 14 | Ukmet | 11.9 | 4.7 | 62.3 | 24.5 | 191 | 0.371 |
| 15 | SM01 | 11.0 | 4.3 | 38.2 | 15.0 | 287 | 0.557 |
| 16 | SM02 | 10.9 | 4.3 | 41.6 | 16.4 | 263 | 0.510 |
| 17 | SM03 | 9.9 | 3.9 | 43.3 | 17.0 | 227 | 0.440 |
| 18 | SM04 | 13.4 | 5.3 | 56.6 | 22.3 | 237 | 0.460 |
| 19 | SM05 | 11.6 | 4.6 | 57.5 | 22.6 | 202 | 0.392 |
| 20 | SM06 | 13.7 | 5.4 | 67.9 | 26.7 | 202 | 0.392 |
| 21 | Happy Valley | 18.6 | 7.3 | 70.0 | 27.6 | 266 | 0.516 |
| 22 | HV1 | 18.3 | 7.2 | 78.0 | 30.7 | 235 | 0.456 |
| 23 | HV2 | 11.7 | 4.6 | 55.1 | 21.7 | 213 | 0.413 |
| 24 | HV3 | 17.2 | 6.8 | 68.8 | 27.1 | 250 | 0.485 |
| 25 | HV4 | 15.3 | 6.0 | 61.6 | 24.3 | 250 | 0.485 |
| 26 | HV5 | 18.8 | 7.4 | 87.1 | 34.3 | 216 | 0.419 |
| 27 | HV6 | 12.3 | 4.8 | 49.8 | 19.6 | 248 | 0.481 |
| 28 | Wkmet | 7.8 | 3.1 | 41.7 | 16.4 | 188 | 0.365 |
| 29 | WK1 | 10.0 | 3.9 | 48.0 | 18.9 | 209 | 0.405 |
| 30 | WK2 | 8.8 | 3.5 | 47.6 | 18.7 | 186 | 0.361 |
| 31 | WK3 | 23.1 | 9.1 | 90.4 | 35.6 | 255 | 0.495 |
| 32 | WK4 | 6.1 | 2.4 | 37.3 | 14.7 | 164 | 0.318 |
| 33 | WK5 | 31.4 | 12.4 | 93.3 | 36.7 | 336 | 0.652 |
| 34 | WK6 | 14.2 | 5.6 | 47.0 | 18.5 | 302 | 0.586 |
| 35 | WK8 | 8.7 | 3.4 | 38.1 | 15.0 | 230 | 0.446 |
| 36 | WK9 | 3.8 | 1.5 | 17.8 | 7.0 | 214 | 0.415 |
| 37 | WK10 | 12.4 | 4.9 | 58.2 | 22.9 | 230 | 0.446 |
| 38 | Sagwon | 7.5 | 3.0 | 31.3 | 12.3 | 213 | 0.413 |
| 39 | H02 | 5.9 | 2.3 | 25.1 | 9.9 | 233 | 0.452 |
| 40 | IB | 11.9 | 4.7 | 44.5 | 17.5 | 267 | 0.518 |
| 41 | MI6 | 11.5 | 4.5 | 45.9 | 18.1 | 252 | 0.489 |
| 42 | MI7 | 8.8 | 3.5 | 40.0 | 15.7 | 219 | 0.425 |
| 43 | DFR1 | 10.5 | 4.1 | 47.0 | 18.5 | 224 | 0.435 |
| 44 | DFM2 | 0.8 | 0.3 | 2.8 | 1.1 | 271 | 0.526 |
| 45 | DFM1 | 10.4 | 4.1 | 48.6 | 19.1 | 215 | 0.417 |
|  | Average | 11.5 | 4.5 | 48.8 | 19.2 | 237 | 0.460 |

Appendix B3. Summary for the sites located on the Coastal Plain.

| № | ID | $\begin{gathered} \text { SWE } \\ \mathrm{cm} \end{gathered}$ | in | SNOW DEPTH |  | SNOW DENSITY |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | cm | in | $\mathrm{kg} / \mathrm{m}^{3}$ | slug/ft ${ }^{3}$ |
| 1 | West Dock | 5.8 | 2.3 | 23.3 | 9.2 | 248 | 0.481 |
| 2 | Franklin Bluffs | 6.6 | 2.6 | 27.6 | 10.9 | 239 | 0.464 |
| 3 | FB1 | 15.1 | 5.9 | 57.9 | 22.8 | 260 | 0.504 |
| 4 | FB2 | 7.8 | 3.1 | 38.2 | 15.0 | 200 | 0.388 |
| 5 | FB3 | 8.8 | 3.5 | 43.1 | 17.0 | 230 | 0.446 |
| 6 | FB4 | 11.3 | 4.4 | 49.6 | 19.5 | 230 | 0.446 |
| 7 | FB5 | 9.6 | 3.8 | 41.2 | 16.2 | 230 | 0.446 |
| 8 | FB6 | 7.9 | 3.1 | 40.6 | 16.0 | 190 | 0.369 |
| 9 | FB7 | 6.5 | 2.6 | 36.2 | 14.3 | 180 | 0.349 |
| 10 | FB8 | 14.4 | 5.7 | 49.3 | 19.4 | 290 | 0.563 |
| 11 | FB9 | 8.3 | 3.3 | 36.3 | 14.3 | 230 | 0.446 |
| 12 | FB10 | 10.1 | 4.0 | 45.7 | 18.0 | 220 | 0.427 |
| 13 | P01 | 6.1 | 2.4 | 18.4 | 7.2 | 331 | 0.642 |
| 14 | P02 | 3.7 | 1.5 | 21.3 | 8.4 | 176 | 0.341 |
| 15 | P03 | 6.5 | 2.6 | 29.0 | 11.4 | 224 | 0.435 |
| 16 | P04 | 5.5 | 2.2 | 22.1 | 8.7 | 250 | 0.485 |
| 17 | P05/BettyP | 6.7 | 2.6 | 30.0 | 11.8 | 224 | 0.435 |
| 18 | P06 | 3.3 | 1.3 | 11.4 | 4.5 | 289 | 0.561 |
| 19 | P07 | 3.8 | 1.5 | 25.1 | 9.9 | 153 | 0.297 |
| 20 | P08 | 4.5 | 1.8 | 19.1 | 7.5 | 236 | 0.458 |
| 21 | MI1 | 5.2 | 2.0 | 21.0 | 8.3 | 249 | 0.483 |
| 22 | MI2 | 7.1 | 2.8 | 30.4 | 12.0 | 235 | 0.456 |
| 23 | MI3 | 5.1 | 2.0 | 15.2 | 6.0 | 339 | 0.658 |
| 24 | MI4 | 5.4 | 2.1 | 28.6 | 11.3 | 189 | 0.367 |
| 25 | MI5 | 7.0 | 2.8 | 32.5 | 12.8 | 215 | 0.417 |
| 26 | H01 | 10.6 | 4.2 | 37.8 | 14.9 | 281 | 0.545 |
| 27 | H03 | 8.0 | 3.1 | 47.3 | 18.6 | 170 | 0.330 |
| 28 | H04 | 20.0 | 7.9 | 84.3 | 33.2 | 240 | 0.466 |
| 29 | H05 | 9.5 | 3.7 | 40.0 | 15.7 | 240 | 0.466 |
| 30 | L30 | 9.4 | 3.7 | 45.4 | 17.9 | 210 | 0.407 |
| 31 | L31 | 9.8 | 3.9 | 46.6 | 18.3 | 210 | 0.407 |
| 32 | L34 | 4.1 | 1.6 | 27.0 | 10.6 | 150 | 0.291 |
| 33 | NK4 | 4.7 | 1.9 | 18.2 | 7.2 | 260 | 0.504 |
| 34 | WC1 | 6.9 | 2.7 | 28.5 | 11.2 | 240 | 0.466 |
| 35 | WK7 | 9.9 | 3.9 | 47.7 | 18.8 | 207 | 0.402 |
| 36 | DFM3 | 16.7 | 6.6 | 62.4 | 24.6 | 270 | 0.524 |
| 37 | DFM4 | 11.6 | 4.6 | 53.8 | 21.2 | 220 | 0.427 |
| 38 | KDA | 6.4 | 2.5 | 24.3 | 9.6 | 265 | 0.514 |
| 39 | MSB | 4.5 | 1.8 | 12.0 | 4.7 | 378 | 0.733 |
| 40 | LFH0701-L | 8.1 | 3.2 | 26.2 | 10.3 | 310 | 0.601 |
| 41 | LFH0701 | 10.2 | 4.0 | 36.6 | 14.4 | 280 | 0.543 |
| 42 | LFH0703-L | 8.1 | 3.2 | 24.4 | 9.6 | 330 | 0.640 |
| 43 | LFH0703 | 6.3 | 2.5 | 28.5 | 11.2 | 220 | 0.427 |
| 44 | LFH0702-L | 9.4 | 3.7 | 27.4 | 10.8 | 340 | 0.660 |
| 45 | LFH0702 | 7.7 | 3.0 | 36.4 | 14.3 | 210 | 0.407 |
| 46 | LFH0705-L | 8.6 | 3.4 | 32.1 | 12.6 | 270 | 0.524 |
| 47 | LFH0705 | 12.3 | 4.8 | 44.7 | 17.6 | 280 | 0.543 |
| 48 | LFH0704 | 5.3 | 2.1 | 19.5 | 7.7 | 274 | 0.532 |
|  | Average | 8.1 | 3.2 | 34.3 | 13.5 | 244 | 0.473 |

Appendix B4. Adjusted SWE for the sites located on the Coastal Plain.

| № | ID | $\begin{gathered} \text { SWE } \\ \mathrm{cm} \end{gathered}$ | in | $\begin{gathered} \text { CORRECTION } \\ \text { FACTOR } \end{gathered}$ | ADJUSTED SWE |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | cm | in |
| 1 | West Dock | 5.8 | 2.3 | 1.12 | 6.5 | 2.6 |
| 2 | Franklin Bluffs | 6.6 | 2.6 | 1.32 | 8.7 | 3.4 |
| 3 | FB1 | 15.1 | 5.9 | not applicable | 15.1 | 5.9 |
| 4 | FB2 | 7.8 | 3.1 | not applicable | 7.8 | 3.1 |
| 5 | FB3 | 8.8 | 3.5 | not applicable | 8.8 | 3.5 |
| 6 | FB4 | 11.3 | 4.4 | not applicable | 11.3 | 4.4 |
| 7 | FB5 | 9.6 | 3.8 | not applicable | 9.6 | 3.8 |
| 8 | FB6 | 7.9 | 3.1 | not applicable | 7.9 | 3.1 |
| 9 | FB7 | 6.5 | 2.6 | not applicable | 6.5 | 2.6 |
| 10 | FB8 | 14.4 | 5.7 | not applicable | 14.4 | 5.7 |
| 11 | FB9 | 8.3 | 3.3 | not applicable | 8.3 | 3.3 |
| 12 | FB10 | 10.1 | 4.0 | not applicable | 10.1 | 4.0 |
| 13 | P01 | 6.1 | 2.4 | 1.43 | 8.7 | 3.4 |
| 14 | P02 | 3.7 | 1.5 | 1.43 | 5.3 | 2.1 |
| 15 | P03 | 6.5 | 2.6 | 1.43 | 9.3 | 3.7 |
| 16 | P04 | 5.5 | 2.2 | 1.43 | 7.9 | 3.1 |
| 17 | P05/BettyP | 6.7 | 2.6 | 1.43 | 9.6 | 3.8 |
| 18 | P06 | 3.3 | 1.3 | 1.43 | 4.7 | 1.9 |
| 19 | P07 | 3.8 | 1.5 | 1.43 | 5.4 | 2.1 |
| 20 | P08 | 4.5 | 1.8 | 1.43 | 6.4 | 2.5 |
| 21 | MI1 | 5.2 | 2.0 | 1.32 | 6.9 | 2.7 |
| 22 | MI2 | 7.1 | 2.8 | 1.32 | 9.4 | 3.7 |
| 23 | MI3 | 5.1 | 2.0 | 1.32 | 6.7 | 2.7 |
| 24 | MI4 | 5.4 | 2.1 | 0.0 | 5.4 | 2.1 |
| 25 | MI5 | 7.0 | 2.8 | 1.32 | 9.2 | 3.6 |
| 26 | H01 | 10.6 | 4.2 | 1.10 | 11.7 | 4.6 |
| 27 | H03 | 8.0 | 3.1 | not applicable | 8.0 | 3.1 |
| 28 | H04 | 20.0 | 7.9 | not applicable | 20.0 | 7.9 |
| 29 | H05 | 9.5 | 3.7 | not applicable | 9.5 | 3.7 |
| 30 | L30 | 9.4 | 3.7 | not applicable | 9.4 | 3.7 |
| 31 | L31 | 9.8 | 3.9 | not applicable | 9.8 | 3.9 |
| 32 | L34 | 4.1 | 1.6 | not applicable | 4.1 | 1.6 |
| 33 | NK4 | 4.7 | 1.9 | not applicable | 4.7 | 1.9 |
| 34 | WC1 | 6.9 | 2.7 | not applicable | 6.9 | 2.7 |
| 35 | WK7 | 9.9 | 3.9 | not applicable | 9.9 | 3.9 |
| 36 | DFM3 | 16.7 | 6.6 | not applicable | 16.7 | 6.6 |
| 37 | DFM4 | 11.6 | 4.6 | not applicable | 11.6 | 4.6 |
| 38 | KDA | 6.4 | 2.5 | 1.43 | 9.2 | 3.6 |
| 39 | MSB | 4.5 | 1.8 | 1.43 | 6.4 | 2.5 |
| 40 | LFH0701-L | 8.1 | 3.2 | 1.34 | 10.9 | 4.3 |
| 41 | LFH0701 | 10.2 | 4.0 | 1.34 | 13.7 | 5.4 |
| 42 | LFH0703-L | 8.1 | 3.2 | 1.19 | 9.6 | 3.8 |
| 43 | LFH0703 | 6.3 | 2.5 | 1.19 | 7.5 | 3.0 |
| 44 | LFH0702-L | 9.4 | 3.7 | 1.19 | 11.2 | 4.4 |
| 45 | LFH0702 | 7.7 | 3.0 | 1.19 | 9.2 | 3.6 |
| 46 | LFH0705-L | 8.6 | 3.4 | not applicable | 8.6 | 3.4 |
| 47 | LFH0705 | 12.3 | 4.8 | not applicable | 12.3 | 4.8 |
| 48 | LFH0704 | 5.3 | 2.1 | 1.19 | 6.3 | 2.5 |
|  | Average | 8.1 | 3.2 |  | 9.1 | 3.6 |

Sites that were sampled after storm are marked as "not applicable", i.e. correction is not needed.

APPENDIX C. HISTORICAL ABLATION DATA

Appendix C1. Snow water equivalent (cm) in the Imnavait Creek basin (basin average).

| Day of Year | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 00 | 01 | 02 | 03 | 04 | 05 | 06 | 07 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 120 |  |  |  |  |  |  |  |  |  |  | 14 |  |  |  |  |  |  |  |  |  |  |  |  |
| 121 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 122 |  |  |  |  |  |  |  |  |  | 8 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 123 |  |  |  | 7.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 124 |  |  |  |  |  |  | 8.2 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 125 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 126 |  |  |  |  |  |  |  |  |  | 4.6 | 6.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| 127 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 12 |  |  |
| 128 | 10.6 |  |  |  |  |  |  |  |  | 1.7 | 5.3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 129 | 10.3 |  | 10 | 6.9 |  | 9.9 | 1.1 |  |  |  |  |  |  |  |  |  |  |  | 15.7 | 12.0 |  |  |  |
| 130 | 9.7 |  | 8.8 | 5.1 |  |  | 0.3 |  |  | 1.3 | 1.3 |  |  |  |  |  |  |  | 14.4 |  |  |  |  |
| 131 | 7.9 |  | 8.6 | 4.8 |  |  | 0.2 |  |  |  |  |  |  |  |  |  |  |  | 14.9 |  |  |  |  |
| 132 |  |  | 7.6 | 1.9 |  | 7.8 | 0.14 |  |  |  |  |  |  |  |  |  |  |  | 14.3 |  |  |  | 11.3 |
| 133 | 8.1 |  | 7.4 | 0.4 |  | 6.9 | 0.12 |  | 10.1 |  |  |  | 12.5 |  | 6.9 |  |  |  | 14.4 |  | 5.7 | 9.6 |  |
| 134 | 7.5 |  | 7.5 | 0.0 |  | 6.5 | 0.06 |  |  | 0.1 |  |  | 10.5 |  | 5.7 |  |  |  | 14.4 | 9.3 | 4.5 |  |  |
| 135 |  |  |  | 0.0 |  | 4.9 | 0 |  |  |  |  |  | 11.0 | 9.5 | 5.1 |  | 13 | 12.4 | 15.1 | 8.2 | 3.3 | 6.8 | 12.4 |
| 136 |  |  | 7.7 |  |  | 3.6 |  |  |  | 0 | 0 |  | 7.3 | 8.7 | 3.9 |  |  | 12.2 | 15.1 | 7.8 | 1.4 |  | 11.0 |
| 137 |  |  | 7.5 |  | 13 | 1.8 |  |  | 5.8 |  |  | 10.1 | 5.8 | 6.5 | 3.6 |  |  | 12.6 | 15.4 | 6.0 | 2.1 | 4.0 | 11.3 |
| 138 | 8.0 |  | 6.9 |  |  | 1.1 |  |  | 0.7 |  |  |  | 5.3 | 6.2 | 3.2 |  | 13 | 12.1 | 14.8 | 4.3 |  | 3.4 | 11.1 |
| 139 | 7.3 |  | 5.2 |  | 12.3 | 0.4 |  |  | 0.1 |  |  |  | 4.5 | 4.2 | 2.2 | 11.2 | 14 | 11.2 | 15.2 | 2.0 | 1.8 | 2.9 | 10.4 |
| 140 | 6.9 |  | 3.9 |  | 12.0 | 0.02 |  |  | 0.0 |  |  | 10.2 | 3.7 | 1.5 | 1.1 | 10.7 |  | 11.1 | 15.4 | 2.1 | 2.1 | 1.3 |  |
| 141 | 6.2 |  | 2.6 |  | 12.0 | 0.0 |  |  |  |  |  |  | 2.8 | 1.5 | 0.6 | 10.2 | 14 | 9.3 | 18.5 | 1.8 | 1.0 | 0.3 | 9.5 |
| 142 | 6.2 |  | 1 |  | 11.4 |  |  |  |  |  |  |  | 2.2 | 0.1 | 0.4 | 9.2 |  | 7.0 | 18.4 | 1.1 | 0.9 | 0.5 | 9.4 |
| 143 | 5.7 |  | 0.2 |  | 10.7 |  |  |  |  |  |  | 10.2 | 1.9 | 0.0 |  | 9.5 | 14 | 5.4 | 16.4 | 0.2 | 0.8 | 0.1 | 6.7 |
| 144 | 4.4 |  | 0.0 |  | 10.5 |  |  | 15.3 |  |  |  | 9.0 | 1.4 |  |  | 9.3 |  | 0.5 | 15.3 | 0.0 | 0.4 | 0.0 | 5.0 |
| 145 | 1.8 |  |  |  | 9.3 |  |  |  |  |  |  | 6.6 | 0.7 |  |  | 8.0 | 14 | 0.0 | 17.1 |  | 0.2 |  | 3.0 |
| 146 | 0.9 |  |  |  | 8.6 |  |  | 14.6 |  |  |  | 4.8 | 0.4 |  |  | 7.5 | 13 |  | 17.3 |  | 0.1 |  | 1.8 |
| 147 | 0.6 | 11.4 |  |  | 7.6 |  |  | 13.9 |  |  |  | 2.6 | 2.5 |  |  | 7.3 | 12 |  | 15.1 |  | 0.0 |  | 0.9 |
| 148 | 0.3 | 11.2 |  |  | 4.5 |  |  | 13.9 |  |  |  |  | 2.2 |  |  | 6.4 | 12 |  | 15.3 |  |  |  | 0.2 |
| 149 | 0.1 | 10.2 |  |  | 2.0 |  |  | 14.1 |  |  |  | 1.6 | 2.2 |  |  | 3.9 | 12 |  | 14.5 |  |  |  | 0.0 |
| 150 | 0.0 | 10.2 |  |  | 0.0 |  |  | 13.7 |  |  |  | 0.4 | 0.8 |  |  | 0.2 | 9.6 |  | 12.8 |  |  |  |  |
| 151 |  | 8.9 |  |  |  |  |  | 13.0 |  |  |  |  | 0.6 |  |  | 0.01 | 4.6 |  | 11.4 |  |  |  |  |
| 152 |  | 7.4 |  |  |  |  |  | 10.8 |  |  |  | 0.0 | 0.0 |  |  | 0.0 | 6.0 |  | 11.7 |  |  |  |  |
| 153 |  | 5.1 |  |  |  |  |  | 9.7 |  |  |  |  |  |  |  |  | 5.9 |  | 7.2 |  |  |  |  |
| 154 |  | 4.1 |  |  |  |  |  | 8.8 |  |  |  |  |  |  |  |  | 3.1 |  | 3.6 |  |  |  |  |
| 155 |  | 2.3 |  |  |  |  |  | 7.5 |  |  |  |  |  |  |  |  | 2.2 |  | 0.4 |  |  |  |  |
| 156 |  | 0.3 |  |  |  |  |  | 5.8 |  |  |  |  |  |  |  |  | 0.8 |  | 0.0 |  |  |  |  |
| 157 |  | 0.0 |  |  |  |  |  | 5.1 |  |  |  |  |  |  |  |  | 0.2 |  |  |  |  |  |  |
| 158 |  |  |  |  |  |  |  | 5.2 |  |  |  |  |  |  |  |  | 0.0 |  |  |  |  |  |  |
| 159 |  |  |  |  |  |  |  | 4.0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| 160 |  |  |  |  |  |  |  | 2.7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 161 |  |  |  |  |  |  |  | 1.0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 162 |  |  |  |  |  |  | 0.0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 163 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Appendix C2. Snow water equivalent (cm) at the Upper Kuparuk (UK) site

| Day of Year | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 00 | 01 | 02 | 03 | 04 | 05 | 06 | 07 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 15 |  | 10 | 14 | 18 | 18 |  | 12 |
| 121 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 122 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 123 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 124 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 125 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 126 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 127 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 128 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 129 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 17.4 |  |  |  |  |
| 130 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 17.0 |  |  |  |  |
| 131 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 15.3 |  | 13.0 |  |  |
| 132 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 12.3 |  | 11.5 |  |  |
| 133 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 11.9 |  |  |  |  |  |  | 12.4 |  |
| 134 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 9.1 |  |  | 12.9 |  | 16.4 | 6.0 |  |  |
| 135 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4.3 |  | 17 | 12.5 | 18.3 | 17.0 | 13.2 |  |  |
| 136 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 3.0 |  |  | 15.3 | 17.4 |  |  | 8.0 | 14.2 |
| 137 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2.5 |  |  |  |  |  | 9.1 | 7.8 |  |
| 138 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.0 |  |  | 15.2 | 18.1 | 11.5 |  | 6.4 | 13.0 |
| 139 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 14 |  | 18.7 | 9.8 | 7.2 | 4.5 | 13 |
| 140 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 20.5 | 16 |  |  | 7.7 | 8.1 | 1.8 |  |
| 141 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 12.6 |  | 9.2 | 5.5 | 0.0 | 11.8 |
| 142 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 17 |  |  |  | 0.3 |  |  |
| 143 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5.8 |  | 5.9 |  |  | 8.0 |
| 144 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 17 |  | 17.6 |  |  |  | 5.4 |
| 145 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 17.9 | 1.1 |  |  |  |
| 146 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 18 |  | 17.3 | 0.5 |  |  | 3.1 |
| 147 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 15 |  |  |  |  |  | 0.0 |
| 148 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 13 |  | 15.2 |  |  |  |  |
| 149 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 15 |  |  |  |  |  |  |
| 150 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 13.3 |  | 13.1 |  |  |  |  |
| 151 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 17.2 | 10.1 |  |  |  |  |  |  |
| 152 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 13.7 |  | 12.3 |  |  |  |  |
| 153 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 17 | 9.7 |  | 10.6 |  |  |  |  |
| 154 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 7.9 |  |  |  |  |
| 155 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 17 | 0 |  |  |  |  |  |  |
| 156 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 16 |  |  |  |  |  |  |  |
| 157 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 9.8 |  |  |  |  |  |  |  |
| 158 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4.8 |  |  |  |  |  |  |  |
| 159 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1.3 |  |  |  |  |  |  |  |


| 160 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Appendix C3. Snow water equivalent (cm) at the Happy Valley (HV) site.

| Day of Year | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 00 | 01 | 02 | 03 | 04 | 05 | 06 | 07 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 14 | 15 | 13 | 23 | 24 |  | 7.3 |
| 121 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 122 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 123 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 124 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 125 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 126 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 127 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 128 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 129 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 130 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 16.4 |  |  |  |  |
| 131 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 132 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 133 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 22.0 |  |
| 134 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 13.1 |  |  |  |  |  |
| 135 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 28.3 |  |  |
| 136 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 12.5 |  |  |  |  |  |
| 137 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 8.1 |
| 138 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 9.6 |  |  |  |  |  |
| 139 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 15.3 |  |  |  | 17.4 |  | 22.0 |  |
| 140 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 7.4 |  | 19 | 6.7 |  |  | 30.0 |  |  |
| 141 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 17.7 | 14.9 |  |  |  |
| 142 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 10 |  |  | 0.8 |  |  |  | 14.1 | 7.8 |
| 143 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.0 | 11.1 | 14.7 | 28.6 |  |  |
| 144 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 13 |  |
| 145 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 20.2 | 8.2 |  |  | 6.9 |
| 146 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 14 |  |  |  | 26.7 | 8.2 |  |
| 147 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 148 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 11.0 |  | 21 | 7 | 6.3 |
| 149 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 |  |  |  |
| 150 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 16.0 |  |  |  |  | 19 | 4.2 | 5.8 |
| 151 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 24.3 |  |  |  |  |
| 152 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 11.7 |  |  |  | 13 | 0 | 4.7 |
| 153 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 13 |  |  | 4.4 |  |  |  |  |
| 154 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 9.2 |  |  |  | 10 |  | 1.7 |
| 155 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 12 |  |  |  |  |  |  |  |
| 156 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4.1 |  |  |  | 4.3 |  | 0 |
| 157 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 11 |  |  |  |  |  |  |  |
| 158 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 |  |  |  |  |  |  |
| 159 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2.3 |  |  |  |  |  |  |  |


| 160 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Appendix C4. Snow water equivalent (cm) at the Sagwon (SH) site.

| Day of Year | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 00 | 01 | 02 | 03 | 04 | 05 | 06 | 07 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 120 |  |  |  | 8.1 | 23 | 11 | 15 |  | 14 |  |  | 21 | 12 |  |  | 10 | 6.4 | 10 | 8.1 | 11 | 5.5 |  | 7.5 |
| 121 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 122 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 123 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 124 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 125 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 126 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 127 |  |  |  |  |  |  | 4.4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 128 |  |  |  |  |  | 5.0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 129 |  |  |  | 5.4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 130 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 131 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 132 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 133 |  |  |  | 3.9 |  |  | 4.19 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 6.0 |  |
| 134 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 7.9 |  |  |  |  |  |
| 135 |  |  | 5.2 |  |  |  |  |  |  |  |  |  |  |  |  | 7.9 |  |  |  |  | 3.6 |  |  |
| 136 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 7.7 |  |  |  |  |  |
| 137 |  |  |  | 3.9 |  |  |  |  |  |  |  |  |  |  |  | 7.7 |  |  |  |  |  |  | 7.3 |
| 138 |  |  |  | 4.4 |  |  |  |  |  |  |  |  |  |  |  |  |  | 3.3 |  |  |  |  |  |
| 139 |  |  |  |  |  |  |  |  |  |  |  | 1.0 |  |  |  | 3.3 |  |  |  | 8.2 |  | 0.0 |  |
| 140 |  |  |  |  |  | 1.1 |  |  |  |  |  |  |  | 1.7 | 5.8 |  | 8.1 | 0.0 |  |  | 4.3 |  |  |
| 141 |  |  |  | 3.9 |  |  |  |  |  |  |  |  |  |  |  | 0.0 |  |  | 8.4 | 4.8 |  |  |  |
| 142 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 7.7 |  |  |  |  |  |  |  | 7.2 |
| 143 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 10.2 | 4.9 | 3.4 |  |  |
| 144 |  |  |  | 3.8 |  |  |  |  |  |  |  |  | 1.1 |  | 4.1 |  |  |  |  |  |  |  |  |
| 145 |  |  |  |  | 14.9 |  |  |  | 5.8 |  |  |  |  |  |  |  |  |  |  | 2.8 |  |  | 7.1 |
| 146 |  |  |  | 3.7 |  |  |  |  |  |  |  |  |  |  |  |  | 6.6 |  |  |  | 2.9 |  |  |
| 147 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 148 |  |  |  | 3.7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 9.2 |  | 2.2 |  | 7.1 |
| 149 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2.8 |  |  |  |
| 150 |  |  |  | 2.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.3 |  | 6.3 |
| 151 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2.0 |  |  |  |  |
| 152 |  |  |  | 2.4 |  |  |  |  |  |  |  |  |  |  |  |  | 5.7 |  |  | 2.3 | 0 |  | 4.7 |
| 153 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 154 |  |  |  | 1.8 |  |  |  |  |  |  |  |  |  |  |  |  | 1.8 |  |  | 1.3 |  |  | 0 |
| 155 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 156 |  |  |  | 1.7 |  |  |  |  |  |  |  |  |  |  |  |  | 0.5 |  |  | 0.5 |  |  |  |
| 157 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.0 |  |  |  |  |  |  |
| 158 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 |  |  |  |
| 159 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| 160 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 161 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 162 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 163 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Appendix C5. Snow water equivalent (cm) at the Franklin Bluffs (FR) site

| Day of Year | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 00 | 01 | 02 | 03 | 04 | 05 | 06 | 07 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 120 |  |  |  | 9.3 |  | 4.7 | 11.3 |  | 12.7 |  |  |  |  | 6.5 |  | 10 |  | 8.5 | 12 |  | 12 | 10 | 6.6 |
| 121 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 122 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 123 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 124 |  |  |  |  |  |  |  |  |  | 6.1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 125 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 126 |  |  |  |  |  |  |  |  |  |  | 7.0 |  |  |  |  |  |  |  |  |  |  |  |  |
| 127 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 128 |  |  |  |  |  | 5.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 129 |  |  |  | 2.7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 130 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 10.2 |  |  |  |  |
| 131 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 132 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 133 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 134 |  |  |  |  |  |  | 10.7 |  |  |  |  |  |  |  |  |  |  | 8.3 |  |  |  |  |  |
| 135 |  |  | 8.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 12.0 |  |  |
| 136 |  |  |  |  |  |  |  | 8.0 |  |  |  |  |  |  |  |  |  | 6.5 |  |  |  |  |  |
| 137 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 15.6 |  |  |  | 8.7 |
| 138 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4.7 | 17.6 |  |  |  |  |
| 139 |  |  |  |  |  |  |  |  |  |  |  | 6.9 |  |  |  |  |  |  | 19.5 |  |  | 8.1 |  |
| 140 |  |  |  |  |  |  |  |  |  |  |  |  |  | 7.1 |  | 14.5 | 13 | 3.3 | 19.1 | 9.1 | 11.5 |  |  |
| 141 |  |  |  |  |  |  | 10.9 | 6.7 |  |  |  |  |  |  |  |  |  |  | 12.5 |  |  |  |  |
| 142 |  |  |  | 5.4 |  |  |  |  |  |  |  |  |  | 9.1 |  |  |  | 1.0 | 12.3 |  | 12.8 | 5.5 | 8.4 |
| 143 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.0 |  |  |  |  |  |
| 144 |  |  |  |  |  |  | 8.6 |  |  |  |  |  |  | 8.2 |  |  |  |  | 10.0 |  |  | 1.8 |  |
| 145 |  |  |  |  | 22.3 |  |  |  | 14 |  |  |  |  | 9.6 |  |  |  |  | 9.2 | 2.9 |  |  | 7.8 |
| 146 |  |  |  | 4.9 |  |  |  |  |  |  |  |  |  | 9.1 |  |  |  |  |  |  | 12.3 | 0 |  |
| 147 |  |  |  |  |  |  | 8.6 |  |  |  |  |  |  | 8 |  |  |  |  | 11.4 |  |  |  |  |
| 148 |  |  |  | 4.0 |  |  |  |  |  |  |  |  |  | 8.6 |  |  |  |  | 9.4 |  | 11 |  | 6.5 |
| 149 |  |  |  |  |  |  |  |  |  |  |  |  | 22.9 | 7.8 |  |  |  |  |  | 2.9 |  |  |  |
| 150 |  |  |  | 3.4 |  |  |  |  |  |  |  |  |  | 6.9 |  |  |  |  | 7.3 |  | 8 |  | 6.3 |
| 151 |  |  |  |  |  |  | 2.8 |  |  |  |  |  |  | 6.7 |  | 14.7 |  |  | 14.6 |  |  |  |  |
| 152 |  |  |  | 1.6 |  |  |  |  |  |  |  |  |  | 4.7 |  |  | 13.4 |  |  | 2.3 | 6 |  | 5.8 |
| 153 |  |  |  |  |  |  |  |  |  |  |  |  |  | 2.9 |  |  |  |  | 2.6 |  |  |  |  |
| 154 |  |  |  | 0.8 |  |  |  |  |  |  |  |  |  | 1.9 |  |  | 9.6 |  |  | 1.3 | 2.7 |  | 1.9 |
| 155 |  |  |  |  |  |  |  |  |  |  |  |  |  | 1.4 |  | 14 |  |  | 0.5 |  |  |  |  |
| 156 |  |  |  | 0.7 |  |  |  |  |  |  |  |  |  | 0.7 |  |  | 7.7 |  |  | 0.4 | 0.4 |  | 0 |
| 157 |  |  |  |  | 7.7 |  |  |  |  |  |  |  |  | 0 |  |  | 5.5 |  | 0 | 0.4 |  |  |  |
| 158 |  |  |  | 0 |  |  |  |  |  |  |  |  |  |  |  | 9.2 | 4.5 |  |  | 0 | 0 |  |  |
| 159 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 8.2 | 3.5 |  |  |  |  |  |  |


| 160 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 3.5 | 2 |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 161 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2 | 0 |  |  |  |  |  |  |
| 162 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1.2 |  |  |  |  |  |  |  |
| 163 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.3 |  |  |  |  |  |  |  |

Appendix C6. Snow water equivalent (cm) at the Betty Pingo (BM) site

| Day of Year | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 00 | 01 | 02 | 03 | 04 | 05 | 06 | 07 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 12 |  |
| 121 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 122 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 123 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 124 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 125 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 126 |  |  |  |  |  |  |  |  |  |  | 6.6 |  |  |  |  |  |  |  |  |  |  |  |  |
| 127 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 128 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 129 |  |  |  |  |  |  |  |  |  |  | 7.6 |  |  |  |  |  |  |  |  |  |  |  |  |
| 130 |  |  |  |  |  |  |  |  |  |  | 7.1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 131 |  |  |  |  |  |  |  |  |  |  | 6.3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 132 |  |  |  |  |  |  |  |  |  |  | 6.0 |  |  |  |  |  |  |  |  |  |  |  |  |
| 133 |  |  |  |  |  |  |  |  |  |  | 6.0 |  |  |  |  |  |  | 9 |  |  |  |  | 9.3 |
| 134 |  |  |  |  |  |  |  |  |  |  | 5.9 |  |  |  |  |  |  |  |  |  |  |  |  |
| 135 |  |  |  |  |  |  |  |  |  |  | 5.8 |  |  |  | 9.9 |  |  |  |  |  |  |  |  |
| 136 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 8.9 |  |  |  |  |  |
| 137 |  |  |  |  |  |  |  |  |  | 7.3 |  |  | 12.8 |  |  |  |  | 8.3 | 10.9 |  |  |  |  |
| 138 |  |  |  |  |  |  |  |  |  |  |  |  | 12.7 |  |  |  |  | 6.3 | 10.0 |  | 7.0 |  |  |
| 139 |  |  |  |  |  |  |  |  |  |  |  | 4.7 | 12.9 |  |  |  |  | 5.4 | 11.5 | 8.1 |  |  |  |
| 140 |  |  |  |  |  |  |  |  |  | 7.2 |  | 4.4 | 13.3 |  |  |  |  | 4.5 | 12.7 |  | 9.5 |  |  |
| 141 |  |  |  |  |  |  |  |  |  | 6.8 |  | 4.6 | 13.2 |  | 9.3 | 12.8 | 8.3 | 4.5 | 12.6 |  |  |  |  |
| 142 |  |  |  |  |  |  |  |  |  |  |  | 4.3 | 12.6 |  | 8.5 |  |  | 2.7 | 12.7 |  |  |  |  |
| 143 |  |  |  |  |  |  |  |  |  | 4.2 |  | 2.8 | 11.8 |  |  |  |  | 0.6 | 11.3 |  |  |  |  |
| 144 |  |  |  |  |  |  |  |  | 10 | 3 |  | 1.9 | 11.3 |  | 9.2 |  |  | 0.0 | 9.5 | 2.7 |  | 6.3 | 8.2 |
| 145 |  |  |  |  |  |  |  |  | 10 | 1.8 | 5.8 | 1.4 | 13.0 |  | 7.5 |  |  |  |  |  |  |  |  |
| 146 |  |  |  |  |  |  |  |  | 12 | 0.9 | 5.1 | 1.8 | 12.3 |  | 8.1 |  |  |  | 11.1 |  | 10.8 | 2.6 | 8.8 |
| 147 |  |  |  |  |  |  |  |  | 12 | 0.6 | 4.1 | 0.7 | 13.3 |  | 8.5 |  |  |  | 11.8 |  |  |  |  |
| 148 |  |  |  |  |  |  |  |  | 11 | 0.8 | 3.7 | 0.4 |  |  | 7 |  |  |  | 11.8 |  |  | 0 | 9.2 |
| 149 |  |  |  |  |  |  |  |  | 5.5 | 0.4 | 3 |  |  |  | 7.2 |  |  |  | 11.5 | 2.6 |  |  |  |
| 150 |  |  |  |  |  |  |  |  | 3.8 | 0.1 | 2.1 |  |  |  | 7 |  |  |  | 9.8 |  | 5.5 |  | 7 |
| 151 |  |  |  |  |  |  |  |  |  | 0 | 1.3 |  |  |  | 6.8 |  |  |  | 10.1 | 2.6 | 4.4 |  |  |
| 152 |  |  |  |  |  |  |  |  | 0 |  | 0 |  |  |  | 5.7 | 14.9 | 8.8 |  | 8.9 |  | 4.2 |  |  |
| 153 |  |  |  |  |  |  |  |  |  |  | 0 |  |  |  | 5.7 |  |  |  | 7.1 | 1.9 |  |  | 6.4 |
| 154 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4.5 |  | 4.1 |  | 6.5 | 1.3 | 3 |  |  |
| 155 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 3.4 |  |  |  | 1.9 | 1.1 | 2.4 |  | 3.1 |
| 156 |  |  |  |  |  |  |  |  |  |  |  |  | 9.7 |  | 2.9 |  | 3.4 |  | 0.0 | 0.6 | 1.1 |  |  |
| 157 |  |  |  |  |  |  |  |  |  |  |  |  | 6.6 |  | 2.6 | 8.4 | 2 |  |  | 0 | 0.2 |  | 0 |
| 158 |  |  |  |  |  |  |  |  |  |  |  |  | 4.2 |  |  | 6.7 | 1.2 |  |  |  |  |  |  |
| 159 |  |  |  |  |  |  |  |  |  |  |  |  | 3.4 |  |  | 6.2 | 0.9 |  |  |  |  |  |  |


| 160 |  |  |  |  |  |  |  |  |  |  |  |  |  | 1.4 |  |  | 3.8 | 0.7 |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 161 |  |  |  |  |  |  |  |  |  |  |  |  | 0.9 |  |  | 1.7 | 0 |  |  |  |  |  |  |
| 162 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.3 |  |  |  |  |  |  |  |  |
| 163 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.0 |  |  |  |  |  |  |  |  |

Appendix C7. Snow water equivalent (cm) at the West Dock (WD) site

| Day of Year | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 00 | 01 | 02 | 03 | 04 | 05 | 06 | 07 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 6.5 | 5.7 | 7.3 | 18 | 7 | 6.3 |  | 5.8 |
| 121 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 122 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 123 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 124 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 125 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 126 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 127 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 128 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 129 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 130 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 131 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 132 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 133 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 7.7 |  |  |  |  | 6.5 |
| 134 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 135 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 3.7 | 8.8 |  |
| 136 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 7.6 |  |  |  |  |  |
| 137 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 7.7 | 7.3 |  |  |  |  |
| 138 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 6.5 | 9.4 |  |  | 7.3 |  |
| 139 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4.8 |  |  |  |  |  |
| 140 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4.3 | 14.6 | 8.2 | 4.9 |  |  |
| 141 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 10.6 |  | 6.3 | 4.3 | 11.2 |  |  |  |  |
| 142 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 8.9 |  |  | 3.1 | 9.3 |  |  |  |  |
| 143 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1.0 |  |  |  |  |  |
| 144 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 12 |  |  | 0.0 | 11.2 |  |  |  |  |
| 145 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 9.6 |  |  |  |  | 2 |  |  |  |
| 146 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 11 |  |  |  | 9.2 |  | 3.8 |  | 6.2 |
| 147 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 11 |  |  |  | 7.3 |  |  | 4 |  |
| 148 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 11 |  |  |  | 8.9 |  |  |  | 6.0 |
| 149 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 9.1 |  |  |  | 6.6 |  |  | 0 |  |
| 150 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 11 |  |  |  | 10.3 | 2.4 | 3.3 |  | 8.3 |
| 151 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 8.9 | 6.2 |  |  |  |  | 2 |  |  |
| 152 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 8 |  | 6.3 |  | 14.1 | 2.4 | 1 |  |  |
| 153 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 6.8 |  |  |  | 5.7 |  |  |  | 7.1 |
| 154 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 7.6 |  | 4.2 |  | 4.9 | 1 | 0.6 |  |  |
| 155 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5.6 |  |  |  | 4.0 | 1 | 0.2 |  | 4.3 |
| 156 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4.7 | 7.2 | 2.8 |  |  | 0.8 |  |  |  |
| 157 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4.7 | 6.8 | 1.7 |  | 0.4 | 0.4 |  |  | 0 |
| 158 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 3.4 | 5.4 | 0.9 |  |  |  |  |  |  |
| 159 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2.8 | 3.4 | 0.4 |  |  |  |  |  |  |


| 160 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 3.3 | 1.6 | 0.4 |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 161 |  |  |  |  |  |  |  |  |  |  |  |  |  | 1.6 | 0.7 | 0.2 |  |  |  |  |  |  |  |
| 162 |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.5 | 0.6 | 0 |  |  |  |  |  |  |  |
| 163 |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 0 |  |  |  |  |  |  |  |  |


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